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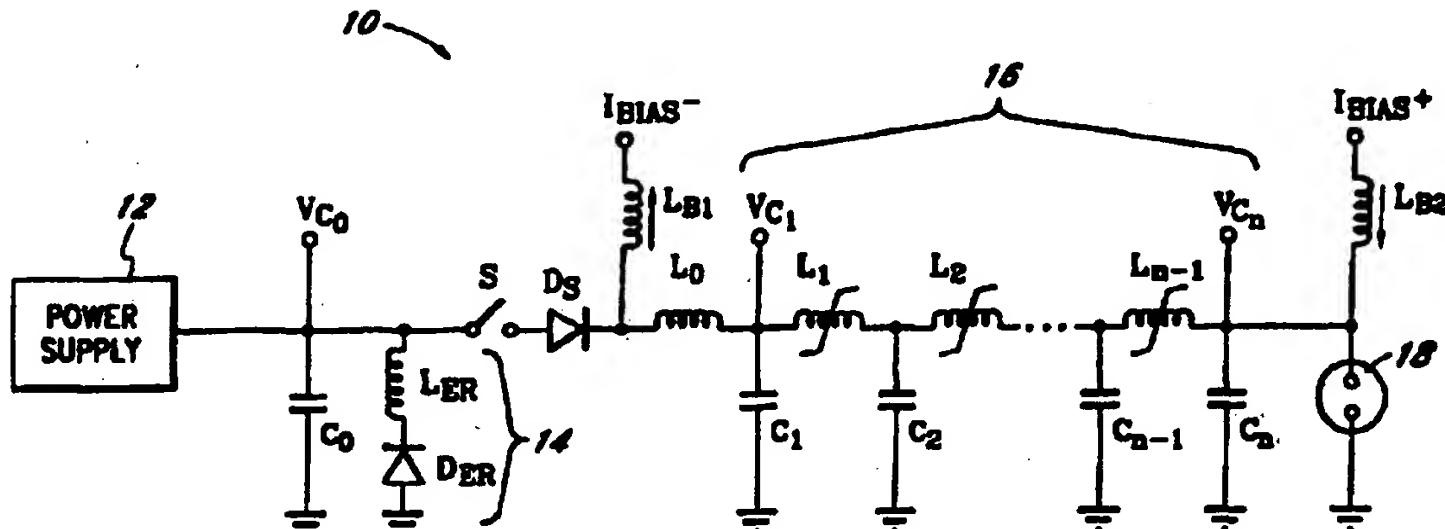
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(71) Applicants: CYMER LASER TECHNOLOGIES [US/US]; 16275 Technology Drive, San Diego, CA 92127-1815 (US). ADVANCED PULSE POWER TECHNOLOGIES, INC. [US/US]; 3300 Crismore Lane, Oakley, CA 94561 (US).			
(72) Inventors: BIRX, Daniel, L.; 3300 Crismore Lane, Route-2 175-D, Oakley, CA 94561 (US). DAS, Palash, P.; 2029 Paseo de Anza, Vista, CA 92084 (US). FOMENKOV, Igor, V.; 7831 Camino Glorita, San Diego, CA 92122 (US). PARTLO, William, N.; Apartment 106, 12055 Alta Camel Court, San Diego, CA 92128 (US). WATSON, Tom, A.; 4427 Salisbury Drive, Carlsbad, CA 92008 (US).		Published <i>With international search report.</i> <i>With amended claims.</i>	
(74) Agents: BLAKELY, Roger, W., Jr. et al.; Blakely, Sokoloff, Taylor & Zafman, 7th floor, 12400 Wilshire Boulevard, Los Angeles, CA 90025-1026 (US).			

(54) Title: PULSE POWER GENERATING CIRCUIT WITH ENERGY RECOVERY



(57) Abstract

A high voltage pulse power generating circuit (10) capable of providing energy recovery is disclosed. The energy efficient pulse generating circuit source comprises a high voltage charge storing element (C) which is periodically discharged into a compressor circuit (16). An energy recovery circuit coupled to the compressor circuit reverses the polarity of the energy dissipated by the pulse power generating circuit (10) and transfers the waste energy back to the power source (12). In a preferred embodiment, the pulse power generating circuit (10) of the present invention utilizes an SCR switch for periodically discharging the charge storing element (C). This embodiment of the present invention provides pulses consistently and will not provide even a single missed pulse.

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PULSE POWER GENERATING CIRCUIT WITH ENERGY RECOVERY

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates generally to pulse power sources and more particularly, to an apparatus and method for providing high voltage pulse power and energy recovery for use in excimer and other pulsed lasers.

2. Description of the Prior Art

In applications where pulsed lasers are operated for extended periods of time, there is a need for energy efficiency, long term reliability and high component lifetimes. In these applications, magnetic compression circuits in conjunction with solid state switches have recently been utilized to supply pulse power because of the reliability and useful life of the magnetic compression circuits and solid state switches.

Such magnetic compression circuits generally utilize a multi-stage LC network to provide the power compression. Various techniques exist for increasing the power output of such devices, including the use of complicated pulse generating networks such as that described in U.S. Patent No. 5,138,622 to Friede et al. and the use of multi-stage magnetic modulators to achieve a high packing factor. These techniques, however, are complex and expensive to implement and their use provide long term unreliability. Specifically, they are energy inefficient and promote short laser component life-times. For example, after the laser discharges, energy left in the circuits is dissipated in the laser, resulting in reduced electrode life.

In addition, the cost of conventional thyratron-based pulse power lasers is high, while the lifetime of the thyratron is limited by cathode and anode erosion. The most serious effect of cathode erosion is a decrease in thyratron switching efficiency. With age, high operating voltages are required to drive the thyratron, which further stresses the thyratron, until eventual replacement is necessary.

Furthermore, anode erosion in conventional thyratron-based pulse power lasers severely reduces the thyratron's high voltage hold-off ability. This causes the thyratron to exhibit occasional prefiring, which results in a premature and weak laser pulse. In applications where high precision is required, such as the manufacture of silicon wafers, prefiring can result in the complete rejection and disposal of the silicon wafers, which is an expensive undertaking.

Accordingly, there is a need in the technology to provide an apparatus and method of increasing the energy efficiency of magnetic compression circuits which is easy to implement, which does not exhibit prefire behavior and which also minimizes electrode erosion.

BRIEF SUMMARY OF THE INVENTION

A high voltage pulse power generating circuit capable of providing energy recovery is disclosed. The energy efficient pulse power generating circuit comprises a high voltage charge storing element which is periodically discharged into a compressor circuit. An energy recovery circuit coupled to the compressor circuit reverses the polarity of energy recovered from the laser by the pulse power generating circuit and transfers the what would have been waste energy back to the power source. In a preferred embodiment, the pulse power generating circuit of the present invention utilizes an SCR switch for periodically discharging the charge storing element. This embodiment of the present invention provides pulses consistently and will not provide even a single missed pulse.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic diagram of a preferred embodiment of the pulse power generating circuit of the present invention.

Figure 2 is a schematic diagram of an alternate embodiment of the pulse power generating circuit of the present invention.

Figure 3 is a graphical representation of the relationship between the flux density and field strength in a typical saturable core inductor.

Figures 4A - 4E are timing diagrams illustrating the energy transfer and recovery cycles in the pulse power generating circuit of the present invention.

Figure 5 is a perspective view of a laser system utilizing the pulse power generating circuit of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

The present invention relates to a pulse power generating circuit which is capable of recovering energy that otherwise would be wasted in a system through a transfer of the dissipated energy back into the power source of the system.

Figure 1 is a schematic diagram of a preferred embodiment of the pulse power generating circuit 10 of the present invention. The pulse power generating circuit 10 comprises a high voltage DC power supply 12, an energy storage capacitor C_0 , an inverting circuit 14, a solid state switch S and a pulse compressor circuit 16 for compressing the duration and increasing the voltage of pulses applied. The pulse power source is coupled to a load 18, typically a pulse discharge load such as an excimer laser.

Figure 2 is a schematic diagram of an alternate embodiment of the pulse power generating circuit 10 illustrated in **Figure 1**. In this alternate embodiment, a step up transformer 20 is coupled to the

output of the compression circuit 16. Alternatively the transformer 20 may instead be coupled to the power generating circuit at one of several nodes (for example, nodes 1, 2, ...n) in the pulse compressor circuit 16, depending on design requirements. A transformer 20 coupled to the circuit 10 at a node closer to the power supply 12 will subject downstream components of the pulse compressor circuit 16 to a higher voltage but lower current than the embodiment of Figure 2, and of course will effect the design of such components because of the different impedance and other operating conditions they will be subjected to. Conversely, a transformer 20 coupled to the circuit 10 at a node closer to the load 18 will allow use of low voltage but high current components supplying the transformer. Further the transformer itself can be somewhat different, depending on its placement, as stepping the voltage up to the desired high level before the final pulse compressor reduces the required peak current capabilities of the transformer.

In a preferred embodiment, the power supply 12 is a 0-1 K volt D.C. power supply, with the pulse power supply providing an energy per pulse of 2 Joules in a pulse width of 100 nanoseconds at approximately a 1 Khz pulse rate. The D.C. supply 12 is used to charge capacitor C_0 , shown as a single capacitor, though typically comprising a bank of parallel connected capacitors. For instance, to obtain a 16 microfarad capacitance for capacitor C_0 , 160 0.1 microfarad, 1000 volt capacitors may be connected in parallel.

The switch S may be a silicon controlled rectifier (SCR), an insulated-gate bipolar transistor (IGBT), a metal-oxide semiconductor field-effect transistor (MOSFET), a MOSFET controlled thyristor (MCT), or any other suitable switching element as known in the technology. The pulse power generating circuit 10 preferably comprises a diode D_s connected in series with the switch S. The inclusion of D_s in the circuit 10 ensures that the circuit 10 is nonconductive with respect to reverse current, as will be described in detail in the section below. In another preferred embodiment, the pulse power source 10 further comprises an inductor L_0 selected in conjunction with C_1 to provide a

time constant for the LC combination to slightly slow the buildup of current flow through the switch S so that the switch may become completely closed prior to high current flow through the switch. This substantially reduces power dissipation in the switch, conserving energy and reducing the heating in the switch and peak current conduction requirement of the switch to reasonably manageable levels. However, it provides a current pulse through the switch which is too low in current and too long in duration to itself provide the intended output for the pulse power source without pulse compressor, provided by the rest of the circuit.

In a preferred embodiment, the switch S is a solid state switch such as an SCR switch. The use of an SCR switch in the pulse power generating circuit 10 of the present invention in a laser offers a distinct advantage. Specifically, it was found that laser systems utilizing the pulse power generating circuit 10 with an SCR switch generate pulses consistently. In fact, the pulse power generating circuit 10 utilizing an SCR switch does not provide even a single missed pulse throughout the life of the laser. This is because SCR switches do not suffer from gradual degradation nor exhibit prefire behavior, as will be discussed in greater detail in the following sections.

The pulse power source 10 also includes bias inductors L_{B1} and L_{B2} , each of which is connected at one end to a current source, I_{BIAS-} and I_{BIAS+} respectively, and at the other end, to compressor circuit 16. As shown in Figure 1, a negative current relative to the desired output pulse is used to bias the compressor circuit 16, as will be discussed in greater detail below. The bias current is supplied through inductors of relatively high inductance to provide relatively high time constants in the bias circuit relative to the pulse rate of the pulse power source to isolate the bias current source from the pulse power source itself. Energy recovery is facilitated in part by inverting circuit 14 which comprises inductor L_{ER} and energy recovery diode D_{ER} .

The compressor circuit 16 comprises banks of capacitors C_1 , C_2 , ... C_{n-1} and C_n and one or more saturable core inductors L_1 , L_2 , ..., L_{n-1}

connected in a ladder network. As shown in **Figure 1**, a first saturable core inductor L_1 is connected between C_1 and C_2 , a second saturable core inductor L_2 may be connected in series between C_2 and C_3, \dots , and a saturable core inductor L_{n-1} is connected in series between C_{n-1} and C_n .

The circuit of **Figure 2** is identical to that of **Figure 1** with the exception of the addition of the step up transformer 20 shown between the output of the pulse power source and the load 18, for the preferred embodiment an excimer laser, though the step up transformer may be inserted in circuit at C_1 or any of the capacitors between C_1 and C_n . The presence and location of the transformer does not effect the function of the other components of the pulse power supply, though being an impedance transforming device (transforming voltages and currents), the values, current capacities and voltage capabilities of the components from and including the power supply 12 to the primary of the transformer will differ substantially from the corresponding components of **Figure 1**, even though the same will normally be chosen to have substantially the same time constants as the embodiment of **Figure 1**.

The method of operation of the present invention will now be discussed. **Figure 3** is a graphical representation of the relationship between the flux density B and magnetizing force per unit length Ni/l characteristic of the major hysteresis loop of a saturable core inductor, where N is the number of inductor coil turns on the core, l is the length of the core and i is the current in the inductor.

In addition, the total flux Φ in the saturable core is given by the equation:

$$\Phi = BA \quad (1)$$

where B is the flux density and A is the cross-sectional area of the core.

As also known in the technology, the relationships between the electromotive force (emf) induced in a coil having N turns, the rate of

change of flux in the core about which the coil is wound and the rate of change in current in the coil are:

$$e = N \frac{d\Phi}{dt} = L \frac{di}{dt} \quad (2)$$

where L is the inductance of the inductor.

Substituting equations (1) into equation (2), we have

$$N \frac{d\Phi}{dt} = N \frac{d(BA)}{dt} \quad (3)$$

Thus,

$$L \frac{di}{dt} = NA \frac{dB}{dt} \quad (4)$$

$$L = NA \frac{dB}{di} \quad (5)$$

Thus, the inductance L of a coil is directly proportional to the rate of change of B with respect to i.

Thus, with reference to Figure 3, the value of $\frac{dB}{di}$ and thus the inductance when the inductor is operating along the line a-b, the line c-d and anywhere along the line c-e of the curve is small, since the gradient of the curve is slight. However, the value of $\frac{dB}{di}$ is large along line b-c and line d-a where the gradient of the curve is steep. Thus, starting at point a (set by the negative bias current I_{BIAS} - see Figures 1 and 2), L is relatively small along line a-b. However, once enough current passes through the inductor coil in the positive direction to start to substantially change the magnetization of the core, the inductance L of the inductor suddenly greatly increases, as shown by the change of $\frac{dB}{di}$ at point b. The inductance remains large until point c is reached, at which time the inductance returns to a low value, allowing the current through the inductor to rapidly rise to point e and beyond, and to later return to point d, all in accordance with the

voltage across the inductor. Between point e and point a, the inductance is again relatively high.

The method of the present invention provides a bias current from I_{BIAS-} and I_{BIAS+} through L_{B1} and L_{B2} to the compression circuit 16 to ensure that the saturation inductors L₁, L₂,...L_{n-1} are biased to operate along line c-e of the curve as shown in **Figure 3**. This ensures that the current passing through saturable inductors L₁, L₂,...L_{n-1} is conducted in one direction for energy recovery. It also ensures a large time constant for each LC stage of the compression circuit 16 so that sufficient time is provided for full energy transfer from one capacitor (e.g., C₁) to another (e.g., C₂) through the inductor (e.g., L₁). At the end of a transfer cycle, the inductors L₁, L₂,...L_{n-1} are biased to ensure that their corresponding inductance is reduced to that at point a in **Figure 3**, so that proper biasing of the inductors L₁, L₂,...L_{n-1} may be accomplished during the next pulsing cycle. Specifically, the inductance of the inductors L₁, L₂,...L_{n-1} must increase with the corresponding increase of positive or uni-directional current in the inductor, as will be discussed in detail below.

The operation of the pulse power generating circuit 10 will be described with reference to **Figure 3** and the timing diagrams illustrated in **Figures 4A-4E**. With the D.C. power supply 12 on prior to the time t₀ (when switch S is open), capacitor C₀ is charged by the current supplied by the D. C. power supply 12. When fully charged, the voltage across capacitor C₀ is V_{C0} (see **Figure 4A**). At t₀, the switch S closes, and the energy stored in capacitor C₀ is transferred to C₁ (see **Figure 4B**) by action of the LC circuit comprising L₀, C₀ and C₁ with a time constant of approximately $\left(\frac{L_0 C_0 C_1}{C_0 + C_1}\right)^{1/2}$, C₁ becoming nearly fully charged and the current in inductor L₀ reducing substantially but still remaining positive at time t₁. Inductor L₀ is included in the circuit to purposely provide a sufficiently large time constant in this energy transfer to ensure that S is fully switched before high currents are encountered, and to limit the maximum current through the switch for a given energy transfer to a value manageable by a solid state switch

by extending the time of the transfer. As capacitor C_0 starts to discharge through switch S and capacitor C_1 begins to charge during this transfer, the current in the coil of saturable inductor L_1 rapidly changes from the negative bias current of point a to the low positive current of point b of **Figure 3**, at which point the inductance jumps to a relative high value to limit the rate of further current increase through L_1 .

At time t_1 , while the current in inductor L_0 is low but still positive, the saturable core of inductor L_1 saturates, at which time the inductance of inductor L_1 jumps to a low value, allowing the current there through to rise to a very high value to transfer the energy from capacitor C_1 to capacitor C_2 with a time constant approximately equal to $\left(\frac{L_{1s}C_1C_2}{C_1+C_2}\right)^{1/2}$, where L_{1s} is the inductance of the inductor L_1 with the core in saturation (line c-e in **Figure 3**). Note that this time constant may be substantially shorter than the time constant $\left(\frac{L_0C_0C_1}{C_0+C_1}\right)^{1/2}$ because L_{1s} may be made much less than L_0 .

In the manner described above, energy is transferred through each stage of the compressor circuit 16, if more than one stage is used, compressing the pulse in time in one or more stages as desired, and if of low voltage originally, being stepped up in voltage where desired. When C_{n-1} is substantially fully charged and the core of inductor L_{n-1} saturates, the energy is coupled through the saturated inductor from C_{n-1} to C_n in a short time period pulse, with the voltage across C_n being applied to the laser 18.

At time t_L , the voltage across C_n builds to the level required to initiate discharge in the laser, and the laser 18 fires. Energy stored in C_n and still being fed to C_n through the inductor is delivered to the laser discharge in the compressed time period of the pulse power supply (see **Figure 4E**). After discharging, C_n is driven negative. When this occurs, L_{n-1} is already saturated for current flow from C_{n-1} to C_n . Thus, instead of having energy ringing in the laser 18, eroding the electrodes, the saturated state of L_{n-1} causes the reverse charge on C_n to be transferred resonantly back into C_{n-1} as shown in **Figure 4D**. This

transfer is accomplished by the continued forward flow of current through L_{n-1} .

When energy is transferred back into C_{n-1} , C_{n-1} is driven negative with respect to C_{n-2} . This process repeats back up the L-C ladder network of the pulse compressor circuit until the energy which would have been destructively dissipated in the load 18, is transferred from C_{n-1} to C_{n-2} . This transfer process continues until the energy in C_n is passed to C_0 , as shown in **Figure 4A**. It should be noted that such reverse energy transfer is possible only if all saturable inductors $L_n, \dots L_{n-1}$ remain forward conducting to operate along curve c-e of **Figure 3**, since the voltage of C_n with respect to C_{n-1} (and similarly, C_{n-1} with respect to C_{n-2}, \dots etc.) must be negative for the energy propagation to be accomplished. Thus, an important factor in the design of the pulse power generating circuit 10 is that all the coils of all saturable inductors $L_1, L_2, \dots L_{n-1}$ must be forwardly conducting to operate in the proper state for one way current transfer until waste energy is fully recovered.

When the waste energy is propagated back into C_0 , C_0 is driven negative with respect to its initially stored charge, and switch S is opened. The inverting circuit 14, comprising an inductor L_{ER} and a solid state diode D_{ER} coupled to ground reverses this polarity through resonant free wheeling - a half cycle of ringing of the $L_{ER}-C_0$ circuit as clamped against reversal of the current in inductor L_{ER} by diode D_{ER} , with the net result that the energy is recovered by the partial recharging of capacitor C_0 , thereby the energy which otherwise would have contributed to erosion of the laser electrodes and reducing the supply requirements of the D.C. power supply.

The pulse power generating circuit of the present invention may be utilized in lasers which operate on the principle of transverse discharge. These lasers include systems which discharge at high pressure, such as CO₂ lasers, copper vapor lasers and excimer lasers including KrF excimer lasers. **Figure 5** illustrates a laser module 20 which may utilize the pulse power generating circuit 10 (enclosed in chassis 22) of the present invention as a power source. A typical

example of such a laser includes the HPL-100 laser module manufactured and sold by Cymer Laser Technologies, assignee of the present invention.

Several advantages exist through the application of the pulse power generating circuit of the present invention. First, by using the pulse power generating circuit, the energy efficiency of a laser system is increased while electrode erosion from after discharge ringing is minimized, since the waste energy which would otherwise be left ringing in the laser 18 is effectively removed from the laser 18. The energy reflected by the laser chamber due to impedance mismatch no longer rings back and forth between the pulse power generating circuit and the laser chamber since this energy is recovered by the pulse power generating circuit of the present invention. As described, the pulse power generating circuit is designed to transmit this reflected energy all the way back through the pulse forming network into C₀. Upon recovery of this energy onto C₀, the switch turns off, ensuring that this captured energy remains in C₀. Thus, regardless of the operating voltage, gas mixture or chamber condition, the voltage waveform across the laser electrodes exhibits the behavior of a well-trained system. This performance is maintained over all laser operating conditions.

As discussed, after-ringing has been found to have a detrimental impact on the laser chamber's electrode lifetime. After the main laser discharge, current flow between the chamber electrodes becomes nonuniform and breaks up into localized areas of high current density called streamers. Elimination of this after-ringing by the solid state pulse power generating circuit starves the streamers of energy and reduces the amount of electrode damage caused by these streamers.

Secondly, by incorporating an SCR switch in a preferred embodiment of the pulse power generating circuit of the present invention, prefiring in the laser system can be eliminated while predictability and reliability of the laser system can be increased. This is because SCR switches, unlike conventional thyratron switches, neither

suffer from gradual degradation nor exhibit prefire behavior. Specifically, the use of SCR switches in pulse power generating circuits has been demonstrated to last for greater than 30 billion pulses under typical operating conditions without a single missed pulse or failure of the pulse power generating circuit. In addition, experimental results in a prototype of the pulse power generating circuit of the present invention has thus far accumulated in excess of 6 billion pulses without a single failure or missed pulse. It has also been determined experimentally that the pulse power generating circuit of the present invention exhibits the same efficiency at 6 billion pulses as it did at 300 million pulses.

Thirdly, the use of the solid state pulse power generating circuit of the present invention in a laser has increased the useful chamber life of the laser by 100%, from 3 billion pulses to 6 billion pulses, without any degradation in performance.

Finally, three other factors are significant in the reduction of cost of operation in using a solid state pulse power generating circuit instead of a thyratron-based pulse power system. The most significant reduction in cost is a ten-fold increase in the expected lifetime of a laser system using the pulse power generating circuit of the present invention. The increase in expected lifetime is from 3 billion pulses for a thyratron pulse power laser system to 30 billion pulses for a solid state pulse power laser system. The second factor in overall system cost reduction is the complete elimination of missed laser pulses and thus the reduction in wafer level rework. The third factor involves a reduction in downtime for laser service procedure. A thyratron-based pulse power circuit used on a typical laser system must go through a 10 minute warm-up period to achieve proper thyratron temperature. The solid state pulse power generating circuit of the present invention requires no warm-up time, and thus each laser service procedure can be shortened by approximately 10 minutes.

Although the invention has been described in terms of a certain preferred embodiment, other embodiments apparent to those skilled

in the art are also within the scope of this invention. Accordingly, the scope of the invention is intended to be defined only by the claims which follow.

CLAIMS:

What is claimed is:

1. A pulse power generating circuit comprising:
a capacitor for storing a charge;
a magnetic pulse compressor circuit;
a switch for periodically applying the charge stored in said capacitor as an input to said compressor circuit, the compressor circuit providing an output pulse in response to the input, said compressor circuit also resonantly providing a reverse charge;
and
an inverting circuit coupled in parallel with said capacitor for inverting said reverse charge to obtain an inverted charge, said inverting circuit also providing said inverted charge to said capacitor.
2. The circuit of Claim 1, wherein said magnetic pulse compressor circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.
3. The circuit of Claim 1, further comprising a linear inductor, said linear inductor being coupled in series with said switch.
4. The circuit of Claim 1, further comprising a second capacitor coupled to said capacitor for storing a charge.
5. The circuit of Claim 1, wherein said inverting circuit comprises an inductor and a diode connected in series.
6. The circuit of Claim 1, further comprising a power source, said power source providing said charge to said capacitor.

7. The circuit of Claim 1, wherein said magnetic pulse compressor circuit is coupled to a load.
8. The circuit of Claim 7, wherein said load is a laser.
9. The circuit of Claim 8, wherein said laser is operable on a transverse discharge.
10. The circuit of Claim 9, wherein said laser is an excimer laser.
11. The circuit of Claim 8, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to the output of said magnetic pulse compressor circuit and said secondary winding being coupled to said load.
12. The circuit of Claim 1, wherein said magnetic pulse compressor circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor coupled to the last stage of said plurality of stages.
13. The circuit of Claim 12, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.
14. A method of generating pulse power, comprising the steps of:
storing a charge in a capacitor;
periodically applying the charge stored as an input to a magnetic pulse compressor circuit;

providing an output pulse in response to the input, said compressor circuit also resonantly providing a reverse charge; recovering said reverse charge by inverting said reverse charge to obtain an inverted charge; and providing said inverted charge to said capacitor.

15. The method of Claim 14, wherein in said periodically applying step, said magnetic pulse compressor circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.

16. The method of Claim 14, wherein said periodically applying step is conducted by means of a switch.

17. The method of Claim 16, further comprising a linear inductor, said linear inductor being coupled to said switch.

18. The method of Claim 14, wherein in said storing step, said capacitor is coupled to a second capacitor.

19. The method of Claim 14, wherein an inverting circuit is used in said recovery step, said inverting circuit comprising an inductor and a diode connected in series.

20. The method of Claim 14, further comprising the step of providing a power source for providing said charge to said capacitor.

21. The method of Claim 14, further comprising the step of providing said output pulse to a load coupled to said magnetic pulse compressor circuit.

22. The method of Claim 21, wherein said load is a laser.

23. The method of Claim 22, further comprising the step of providing said output pulse to a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to the output of said magnetic pulse compressor circuit and said secondary winding being coupled to said load.

24. The method of Claim 14, wherein said magnetic pulse compressor circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor in parallel with the last stage of said plurality of stages.

25. The method of Claim 24, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.

26. A high-voltage pulse power laser system, comprising:
a power source for supplying a charge;
a capacitor for storing said charge;
a magnetic pulse compressor circuit;
a solid state switch for periodically applying the charge stored in said capacitor as an input to said compressor circuit, the compressor circuit providing an output pulse in response to the input, said compressor circuit also resonantly providing a reverse charge;
a laser coupled to said magnetic pulse compressor circuit, said laser receiving said output pulse; and
an inverting circuit coupled in parallel with said capacitor for inverting said reverse charge to obtain an inverted charge, said inverting circuit also providing said inverted charge to said capacitor.

27. The system of Claim 26, further comprising a pair of current bias terminals coupled to said magnetic pulse compressor

circuit, said pair of current bias terminals for providing a bias current to said compressor circuit.

28. The system of Claim 26, wherein said magnetic pulse compressor circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.

29. The system of Claim 26, further comprising a linear inductor, said linear inductor being coupled in series with said switch.

30. The system of Claim 26, further comprising a second capacitor coupled to said capacitor for storing a charge.

31. The system of Claim 26, wherein said inverting circuit comprises an inductor and a diode connected in series.

32. The system of Claim 26, further comprising a power source, said power source providing said charge to said capacitor.

33. The system of Claim 26, wherein said laser is operable on a transverse discharge.

34. The system of Claim 26, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to the output of said magnetic pulse compressor circuit and said secondary winding being coupled to said laser.

35. The system of Claim 26, wherein said magnetic pulse compressor circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor coupled to the last stage of said plurality of stages.

36. The system of Claim 35, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.
37. A high voltage pulse power laser system comprising:
 - a power source;
 - a pulse compressor circuit having a solid state switch coupled to said power source; and
 - a laser coupled to the output of said pulse compressor circuit;said pulse compressor circuit providing compressed power to said laser in response to power input from said power source through the solid state switch, said compressor circuit also recovering energy not used in said laser and returning the recovered energy to said power source.
38. The system of Claim 37, wherein said pulse compressor circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.
39. The system of Claim 37 wherein said pulse compressor circuit further comprises a linear inductor coupled in series with said switch.
40. The system of Claim 37, further comprising a capacitor coupled to said power source for storing energy.
41. The system of Claim 37, wherein said pulse compressor circuit further comprises an inverting circuit, said inverting circuit comprising an inductor and a diode connected in series.

42. The system of Claim 37, wherein said laser is operable on a transverse discharge.

43. The system of Claim 42, wherein said laser is an excimer laser.

44. The system of Claim 37, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to the output of said pulse compressor circuit and said secondary winding being coupled to said laser.

45. The system of Claim 37, wherein said pulse compressor circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor coupled to the last stage of said plurality of stages.

46. The system of Claim 45, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.

47. A method of recovering energy in a laser system, comprising the steps of:

periodically applying a charge as an input to a pulse compressor circuit;

providing an output pulse to said laser system in response to the input, said compressor circuit also resonantly providing a reverse charge;

recovering said reverse charge by inverting said reverse charge to obtain an inverted charge; and

providing said inverted charge in a next output pulse.

48. The method of Claim 47, wherein in said periodically applying step, said pulse compressor circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.

49. The method of Claim 47, wherein said periodically applying step is applied by means of a solid state switch.

50. The method of Claim 49, further comprising a linear inductor, said linear inductor being coupled to said switch.

51. The method of Claim 47, further comprising the step of storing said charge in a capacitor prior to said periodically applying step.

52. The method of Claim 47, wherein an inverting circuit is used in said recovery step, said inverting circuit comprising an inductor and a diode connected in series.

53. The method of Claim 47, further comprising the step of providing a power source for providing said charge.

54. The method of Claim 47, further comprising the step of providing said output pulse to a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to the output of said pulse compressor circuit and said secondary winding being coupled to said load.

55. The method of Claim 47, wherein said pulse compressor circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor in parallel with the last stage of said plurality of stages.

56. The method of Claim 55, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.

57. A high voltage pulse power laser system comprising:
a power source;
a pulse compressor circuit having a solid state switch coupled to said power source; and
a pulse discharge laser coupled to the output of said pulse compressor circuit;
said pulse compressor circuit consistently providing compressed power to said laser without missed pulses in response to power input from said power source through the solid state switch.

58. The system of Claim 57, wherein said compressor circuit also recovers energy not used in said laser and returns the recovered energy to said power source.

59. The system of Claim 57, wherein said laser is a transverse discharge laser.

60. The system of Claim 57, wherein said laser is an excimer laser.

61. The system of Claim 60, wherein said laser is a KrF excimer laser.

62. The system of Claim 57, wherein said pulse compression circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.

63. The system of Claim 57, wherein said pulse compression circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor coupled to the last stage of said plurality of stages.

64. The system of Claim 57, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.

AMENDED CLAIMS

[received by the International Bureau on 15 July 1996 (15.07.96);
original claims 1,5,14,19,26,31,37,41,47,52 and 57 amended;
remaining claims unchanged (10 pages)]

1. A pulse power generating circuit comprising:
a capacitor for storing a charge;
a magnetic pulse compressor circuit;
a switch coupled at one end to said capacitor and another
end to said magnetic pulse compressor circuit, for periodically
applying the charge stored in said capacitor as an input to said
compressor circuit, the compressor circuit providing an output
pulse in response to the input, said compressor circuit also
resonantly providing a reverse charge that is reflected from a
load coupled to said compressor circuit; and
an inverting circuit coupled in parallel with said capacitor
for storing and inverting said reverse charge to obtain an
inverted charge, said inverting circuit also providing said
inverted charge to said capacitor through said switch during a
next pulse.
2. The circuit of Claim 1, wherein said magnetic pulse
compressor circuit comprises at least one stage, said at least one stage
comprising a capacitor and a saturable inductor.
3. The circuit of Claim 1, further comprising a linear
inductor, said linear inductor being coupled in series with said switch.
4. The circuit of Claim 1, further comprising a second
capacitor coupled to said capacitor for storing a charge.
5. The circuit of Claim 1, wherein said inverting circuit
comprises an inductor.

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6. The circuit of Claim 1, further comprising a power source, said power source providing said charge to said capacitor.

7. The circuit of Claim 1, wherein said magnetic pulse compressor circuit is coupled to a load.

8. The circuit of Claim 7, wherein said load is a laser.

9. The circuit of Claim 8, wherein said laser is operable on a transverse discharge.

10. The circuit of Claim 9, wherein said laser is an excimer laser.

11. The circuit of Claim 8, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to the output of said magnetic pulse compressor circuit and said secondary winding being coupled to said load.

12. The circuit of Claim 1, wherein said magnetic pulse compressor circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor coupled to the last stage of said plurality of stages.

13. The circuit of Claim 12, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.

14. A method of generating pulse power, comprising the steps of:

storing a charge in a capacitor;

periodically applying the charge stored as an input to a magnetic pulse compressor circuit;

providing an output pulse in response to the input, said compressor circuit also resonantly providing a reverse charge that is reflected from a load coupled to said magnetic pulse compressor circuit;

recovering said reverse charge by inverting said reverse charge to obtain an inverted charge; and

providing said inverted charge to said capacitor during a next pulse.

15. The method of Claim 14, wherein in said periodically applying step, said magnetic pulse compressor circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.

16. The method of Claim 14, wherein said periodically applying step is conducted by means of a switch.

17. The method of Claim 16, further comprising a linear inductor, said linear inductor being coupled to said switch.

18. The method of Claim 14, wherein in said storing step, said capacitor is coupled to a second capacitor.

19. The method of Claim 14, wherein an inverting circuit is used in said recovery step, said inverting circuit comprising an inductor.

20. The method of Claim 14, further comprising the step of providing a power source for providing said charge to said capacitor.

21. The method of Claim 14, further comprising the step of providing said output pulse to a load coupled to said magnetic pulse compressor circuit.

22. The method of Claim 21, wherein said load is a laser.

23. The method of Claim 22, further comprising the step of providing said output pulse to a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to the output of said magnetic pulse compressor circuit and said secondary winding being coupled to said load.

24. The method of Claim 14, wherein said magnetic pulse compressor circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor in parallel with the last stage of said plurality of stages.

25. The method of Claim 24, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.

26. A high-voltage pulse power laser system, comprising:
a power source for supplying a charge;
a capacitor for storing said charge;
a magnetic pulse compressor circuit;
a solid state switch coupled at one end to said capacitor and at a second end to said magnetic pulse compression circuit, for periodically applying the charge stored in said capacitor as an input to said compressor circuit, the compressor circuit providing an output pulse in response to the input, said compressor circuit also resonantly providing a reverse charge that is reflected from a load coupled to said magnetic pulse compressor circuit;

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a laser coupled to said magnetic pulse compressor circuit, said laser receiving said output pulse; and

an inverting circuit coupled in parallel with said capacitor for storing and inverting said reverse charge to obtain an inverted charge, said inverting circuit also providing said inverted charge to said capacitor through said switch.

27. The system of Claim 26, further comprising a pair of current bias terminals coupled to said magnetic pulse compressor circuit, said pair of current bias terminals for providing a bias current to said compressor circuit.

28. The system of Claim 26, wherein said magnetic pulse compressor circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.

29. The system of Claim 26, further comprising a linear inductor, said linear inductor being coupled in series with said switch.

30. The system of Claim 26, further comprising a second capacitor coupled to said capacitor for storing a charge.

31. The system of Claim 26, wherein said inverting circuit comprises an inductor.

32. The system of Claim 26, further comprising a power source, said power source providing said charge to said capacitor.

33. The system of Claim 26, wherein said laser is operable on a transverse discharge.

34. The system of Claim 26, further comprising a transformer, said transformer having a primary winding and a secondary winding,

said primary winding being coupled to the output of said magnetic pulse compressor circuit and said secondary winding being coupled to said laser.

35. The system of Claim 26, wherein said magnetic pulse compressor circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor coupled to the last stage of said plurality of stages.

36. The system of Claim 35, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.

37. A high voltage pulse power laser system comprising:
a power source;
a pulse compressor circuit having a solid state switch coupled to said power source; and
a laser coupled to the output of said pulse compressor circuit;
said pulse compressor circuit providing compressed power to said laser in response to power input from said power source through the solid state switch, said compressor circuit also recovering energy not used in said laser by reversing the unused energy and returning the recovered energy to said power source.

38. The system of Claim 37, wherein said pulse compressor circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.

39. The system of Claim 37 wherein said pulse compressor circuit further comprises a linear inductor coupled in series with said switch.

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40. The system of Claim 37, further comprising a capacitor coupled to said power source for storing energy.
41. The system of Claim 37, wherein said pulse compressor circuit further comprises an inverting circuit, said inverting circuit comprising an inductor.
42. The system of Claim 37, wherein said laser is operable on a transverse discharge.
43. The system of Claim 42, wherein said laser is an excimer laser.
44. The system of Claim 37, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to the output of said pulse compressor circuit and said secondary winding being coupled to said laser.
45. The system of Claim 37, wherein said pulse compressor circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor coupled to the last stage of said plurality of stages.
46. The system of Claim 45, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.
47. A method of recovering energy in a laser system, comprising the steps of:
periodically applying a charge as an input to a pulse compressor circuit;

providing an output pulse to said laser system in response to the input, said compressor circuit also resonantly providing a reverse charge that is reflected by said laser system;

recovering said reverse charge by inverting said reverse charge to obtain an inverted charge; and

providing said inverted charge as part of the input to said compressor circuit in a next output pulse.

48. The method of Claim 47, wherein in said periodically applying step, said pulse compressor circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.

49. The method of Claim 47, wherein said periodically applying step is applied by means of a solid state switch.

50. The method of Claim 49, further comprising a linear inductor, said linear inductor being coupled to said switch.

51. The method of Claim 47, further comprising the step of storing said charge in a capacitor prior to said periodically applying step.

52. The method of Claim 47, wherein an inverting circuit is used in said recovery step, said inverting circuit comprising an inductor.

53. The method of Claim 47, further comprising the step of providing a power source for providing said charge.

54. The method of Claim 47, further comprising the step of providing said output pulse to a transformer, said transformer having a primary winding and a secondary winding, said primary winding

being coupled to the output of said pulse compressor circuit and said secondary winding being coupled to said load.

55. The method of Claim 47, wherein said pulse compressor circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor in parallel with the last stage of said plurality of stages.

56. The method of Claim 55, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.

57. A high voltage pulse power laser system comprising:
a power source;
a capacitor for storing a charge;
a pulse compressor circuit having a solid state switch coupled to said power source; and
a pulse discharge laser coupled to the output of said pulse compressor circuit;
an inverting circuit coupled in parallel with said capacitor for storing and inverting a reverse charge that is reflected by said pulse discharge laser;
said pulse compressor circuit consistently providing compressed power to said laser without missed pulses in response to power input from said power source through the solid state switch.

58. The system of Claim 57, wherein said compressor circuit also recovers energy not used in said laser and returns the recovered energy to said power source.

59. The system of Claim 57, wherein said laser is a transverse discharge laser.

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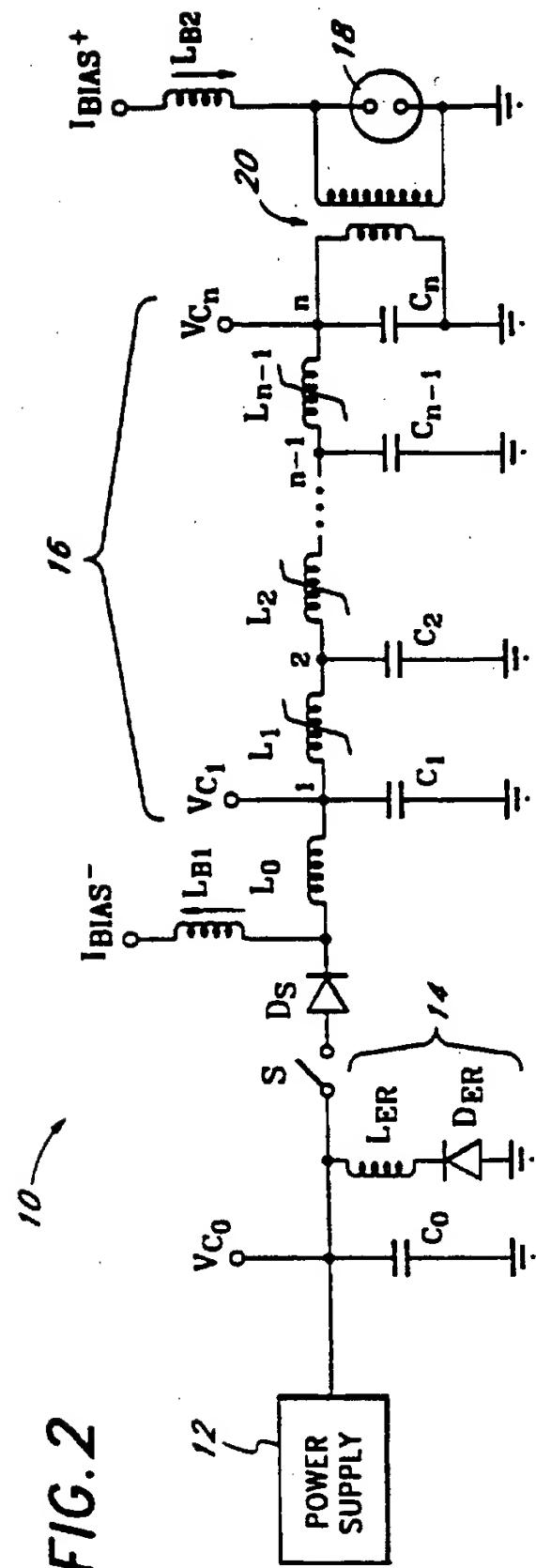
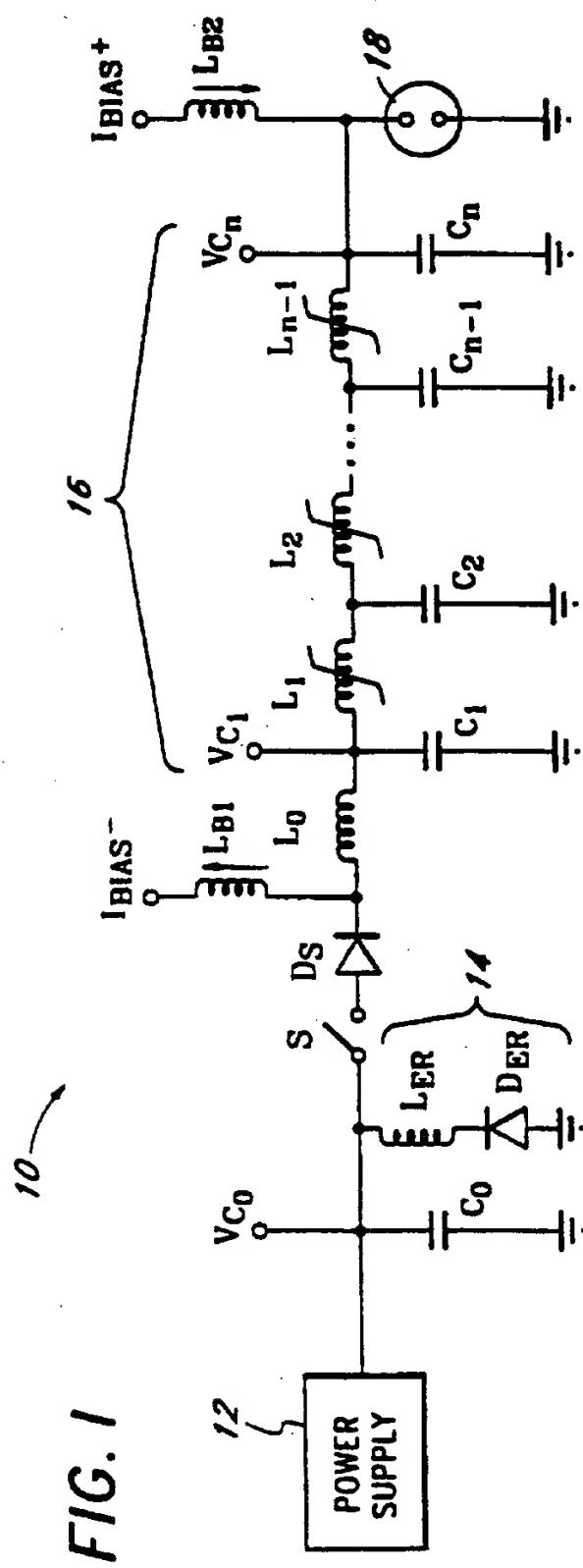
60. The system of Claim 57, wherein said laser is an excimer laser.

61. The system of Claim 60, wherein said laser is a KrF excimer laser.

62. The system of Claim 57, wherein said pulse compression circuit comprises at least one stage, said at least one stage comprising a capacitor and a saturable inductor.

63. The system of Claim 57, wherein said pulse compression circuit comprises a plurality of stages, each of said stages comprising a capacitor and a saturable inductor and an output capacitor coupled to the last stage of said plurality of stages.

64. The system of Claim 57, further comprising a transformer, said transformer having a primary winding and a secondary winding, said primary winding being coupled to one of said stages and said secondary winding being coupled to a next stage.



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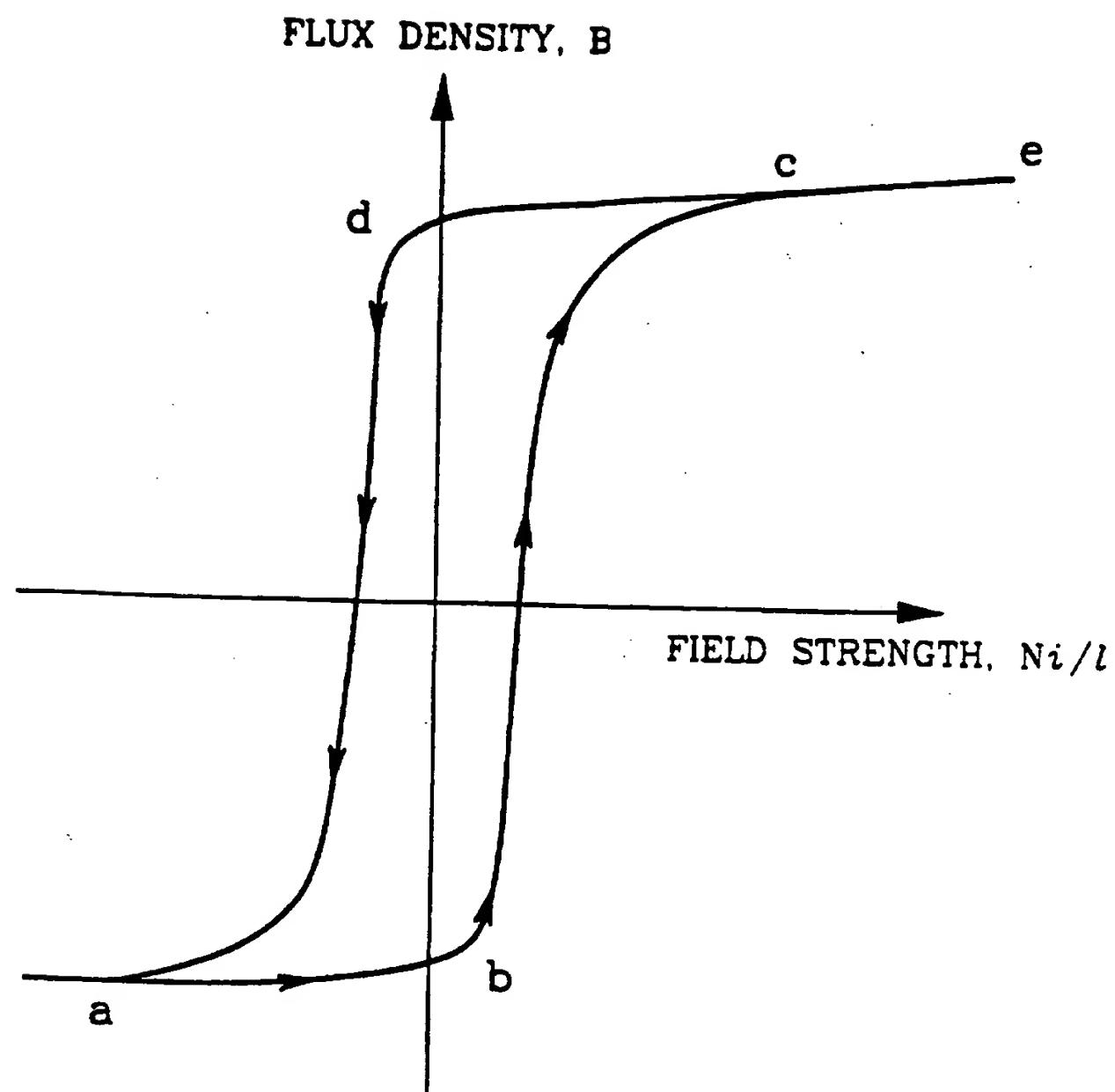


FIG. 3

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FIG. 4A

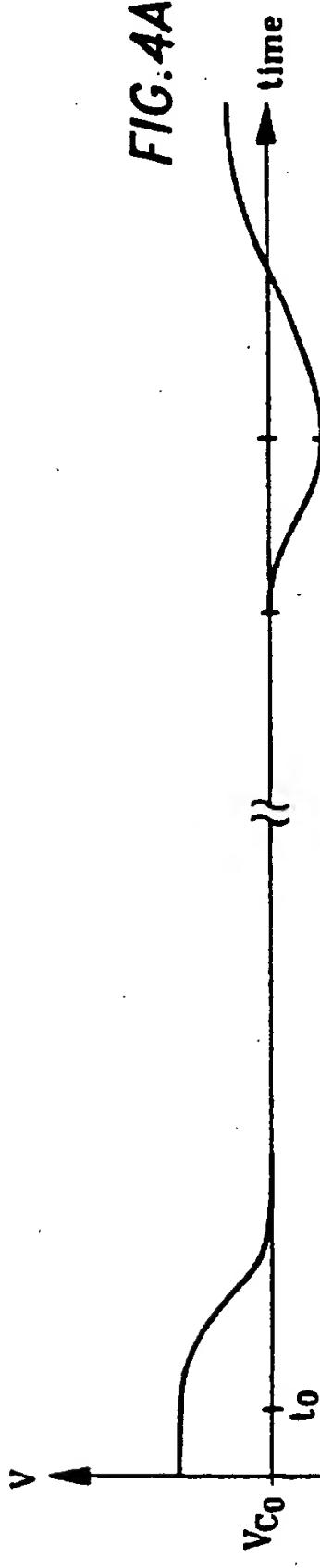


FIG. 4B

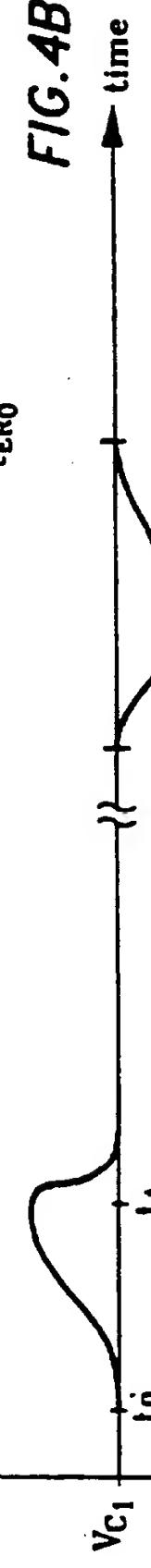


FIG. 4C

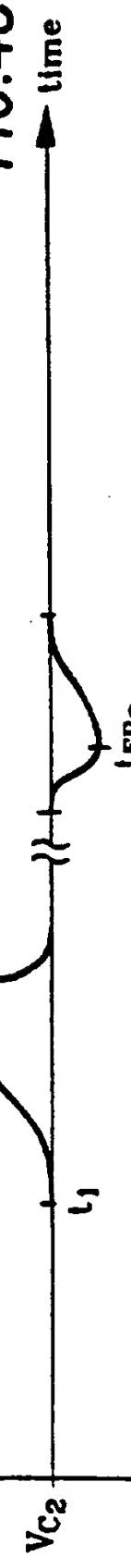


FIG. 4D



FIG. 4E



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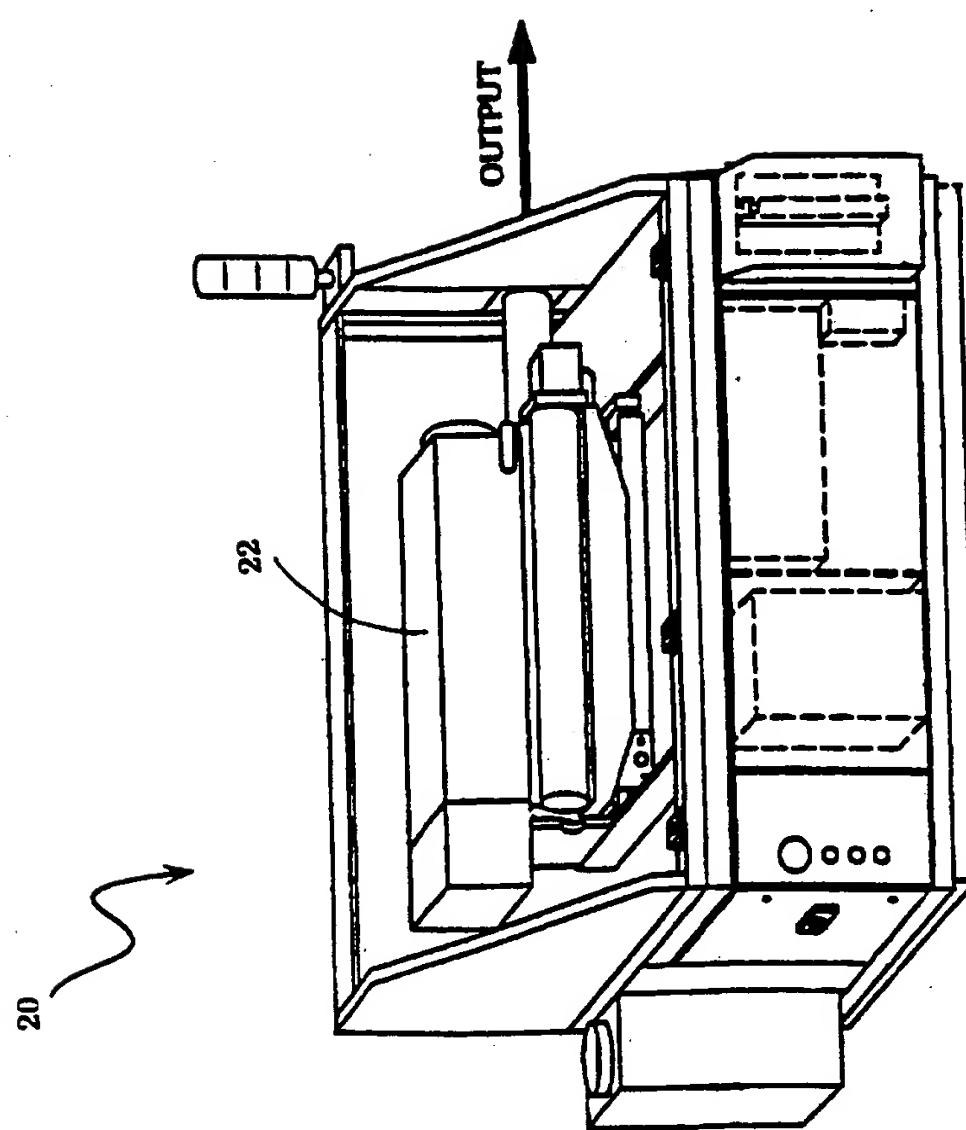


Figure 5

INTERNATIONAL SEARCH REPORT

International application No.

PCT/US96/01033

A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) : HO1S 3/00

US CL : 372/38

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 372/38

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

NONE

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

NONE

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US,A 5,138,622 (FRIEDE ET AL) 11 AUGUST 1992 (SEE ENTIRE DOCUMENT)	1

Further documents are listed in the continuation of Box C.

See patent family annex.

* Special categories of cited documents:	"T"	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
A document defining the general state of the art which is not considered to be of particular relevance	"X"	document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
E earlier document published on or after the international filing date	"Y"	document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
L document which may throw doubt on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"Z"	document member of the same patent family
O document referring to an oral disclosure, use, exhibition or other means		
P document published prior to the international filing date but later than the priority date claimed		

Date of the actual completion of the international search	Date of mailing of the international search report
07 MAY 1996	15 MAY 1996

Name and mailing address of the ISA/US Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231 Facsimile No. (703) 305-3230	Authorized officer LEON SCOTT JR. Telephone No. (703) 308-4884
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